

PLASMA SOURCES FOR MICRO-THRUSTERS*

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AGENDA

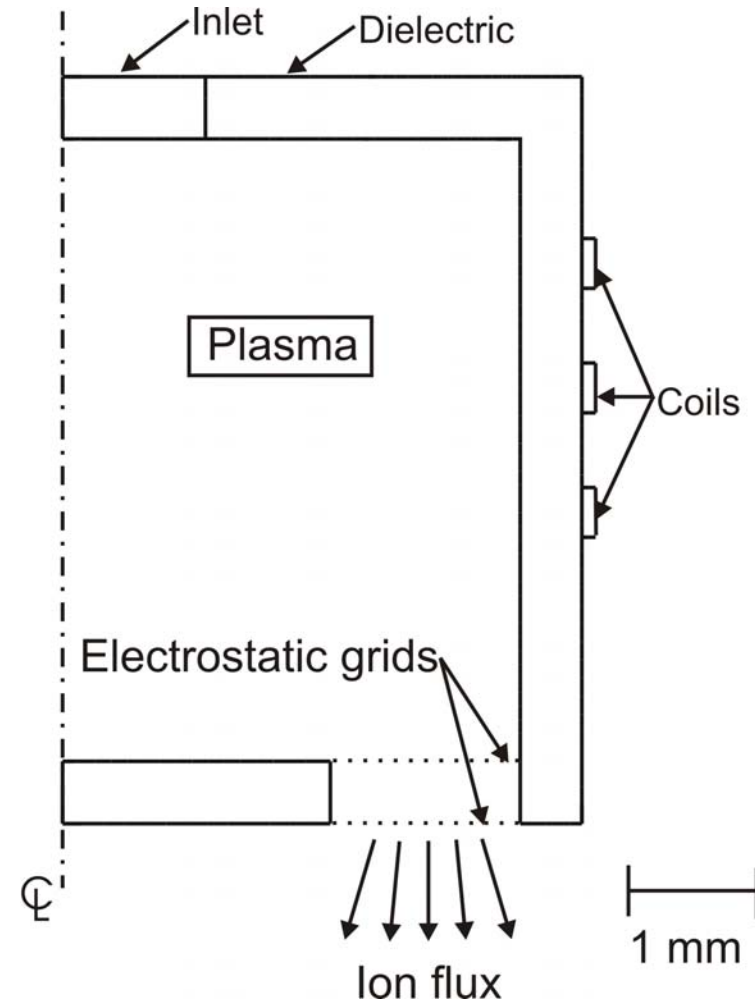
- **Micro-Inductively Coupled Plasma (mICP) discharges:
Applications to thrusters**
- **Description of model**
- **Results**
 - **Validation**
 - **Effect of flow**
 - **Ionization fraction**
 - **Effect of geometry**
 - **Sources of energetic neutrals**
- **Conclusions**

MICRO THRUSTERS

- **Micro-thrusters typically have diameters of a few cm and generate thrusts ranging from sub- μN to mN.**
- **Micro-plasma thrusters have high specific impulse, use inert non-contaminating propellants, and potentially have higher thrust-to-power ratios.**
- **Need to maximize the ionization fraction at low input power and sustain the plasma at high surface-to-volume ratios.**
- **Ionization fractions $\sim 0.1\%$ and higher can be obtained for spherical hollow cathode devices, but similar values have not been reported in mICPs.**

ICP SOURCES: APPLICATIONS TO MICRO-THRUSTERS

- ICPs have potentially longer service lives due to the absence of electrodes.
- Need to operate at high frequencies to keep skin depth reasonably small.
- Scaling to smaller sizes may be limited by sheath width.
- These reactors can also be used as generators of energetic species such as $O_2(^1\Delta)$.



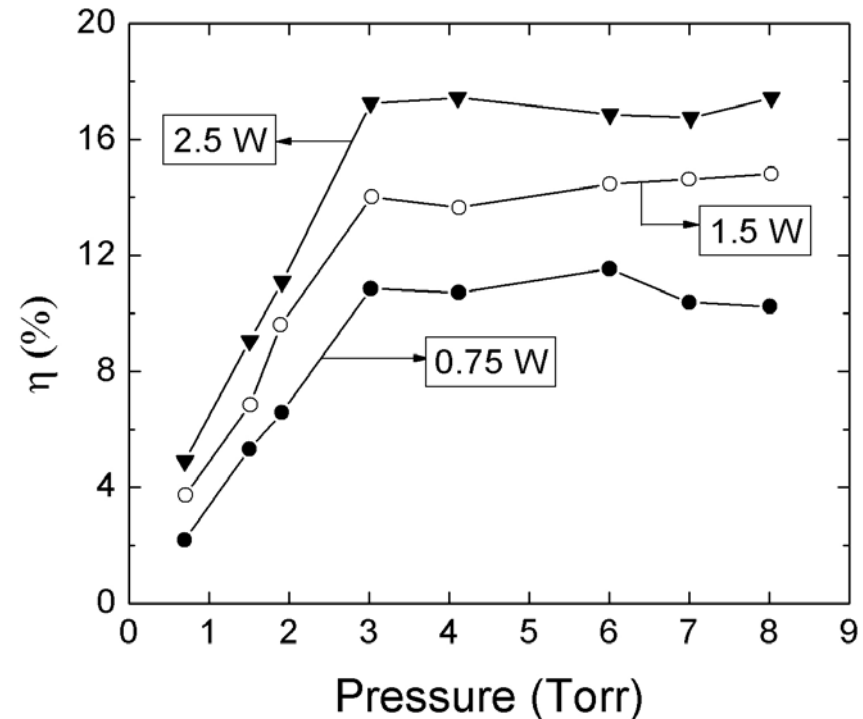
Representative geometry of the reactor

DETAILS OF THIS STUDY

- **Computational investigation of 2-d cylindrically symmetric reactors.**
- **Reactor geometry:**
 - **Radius of 0.3 – 0.5 cm and height of 0.5 – 0.6 cm.**
- **Operating conditions:**
 - **500 mTorr to 8 Torr gas pressures.**
 - **Pure Argon gas and He/O₂ gas mixtures.**
 - **0.5 – 3.0 Watts input power, at 450 MHz for validation.**
 - **0.15 – 1.0 Watts absorbed power, at 493 MHz.**
- **Goals:**
 - **Validate model with experimental data.**
 - **Compute ionization fraction at these conditions.**
 - **Study the effect of geometry on plasma characteristics.**

POWER ABSORPTION EFFICIENCY

- Efficiency defined as power absorbed by the plasma to the input power.
- Efficiency is very low at low pressures because plasma is not collisional enough.
- At higher pressures, efficiency is bounded by losses in the electrical circuit.



- O. B. Minayeva and J. Hopwood, J. Appl. Phys. 94, 2003

MODEL: POTENTIALS AND SOURCES

- Poisson's equation with volume and surface charges for all charged species.

$$-\nabla \cdot \epsilon \nabla \Phi = \rho_v + \rho_s$$

$$\frac{\partial \rho_v}{\partial t} = \sum_i -\nabla \cdot (\mathbf{q}_i \vec{\phi}_i)$$

$$\frac{\partial \rho_s}{\partial t} = \sum_i -\nabla \cdot (\mathbf{q}_i \vec{\phi}_i (1 + \gamma_i)) - \nabla \cdot (\sigma(-\nabla \Phi) + \vec{j}_E)$$

- Source densities due to e-impact, heavy particle reactions, and secondary emissions are included.
- Fluxes discretized using Scharfetter-Gummel technique.

$$\frac{\partial \mathbf{N}_i}{\partial t} = -\vec{\nabla} \cdot \vec{\phi}_i + \mathbf{S}_i \quad \vec{\phi}_{i+1/2} = \alpha \bar{\mathbf{D}} \left(\frac{n_{i+1} - n_i \exp(\alpha \Delta x)}{1 - \exp(\alpha \Delta x)} \right)$$

$$\alpha = \frac{\left(\frac{\mathbf{q}}{|\mathbf{q}|} \right) \bar{\mu} \left(\frac{\Phi_{i+1} - \Phi_i}{\Delta x} \right) - \vec{\mathbf{v}}_{\text{BULK}}}{\bar{\mathbf{D}}}$$

MODEL: TRANSPORT PROPERTIES

- Maxwell's equations were solved for electromagnetic fields and power deposition.

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \nabla \times \left(\frac{\vec{B}}{\mu_0} \right) = \frac{\partial}{\partial t} (\epsilon \vec{E}) + \mathbf{J} \quad \mathbf{P} = \frac{1}{2} (\sigma \vec{E}) \cdot \vec{E}$$

- Navier-Stokes equations for gas velocities, temperature.

Continuity $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = 0$

Momentum $\frac{\partial (\rho \vec{v})}{\partial t} + \nabla \cdot (\rho \vec{v} \vec{v}) = -\nabla p + \nabla \left[\mu \left\{ \nabla \vec{v} + (\nabla \vec{v})^T - \frac{2}{3} (\nabla \cdot \vec{v}) \mathbf{I} \right\} \right] + \bar{\mathbf{S}}_{\text{plasma}}$

Energy $\frac{\partial \rho c_p T}{\partial t} = -\nabla \cdot (\rho c_p \vec{v} T) - \nabla \cdot (\kappa \nabla T) + \mathbf{S}_{\text{plasma}}$

- Electron energy equation coupled with Boltzmann solution for electron transport coefficients.
- Table look-ups of cross-sections for calculating rate coefficients.

MODEL: SOLUTION

- Finite volume techniques were used for 2-d unstructured triangulated meshes.
- Equations solved using implicit time-stepping using an iterative Newton's method with numerically derived Jacobian elements.

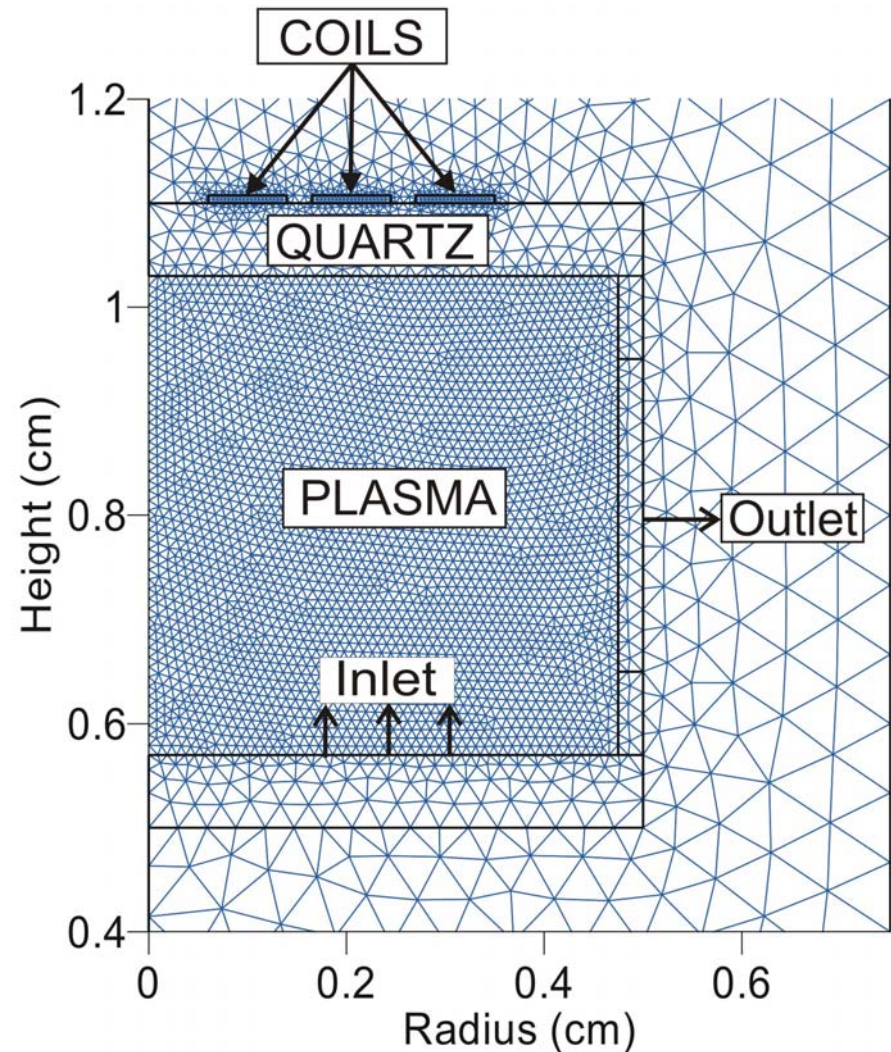
$$\mathbf{N}_i(\mathbf{t} + \Delta\mathbf{t}) = \mathbf{N}_i(\mathbf{t}) + \Delta\mathbf{N}_i\Delta\mathbf{t}$$

$$\Delta\mathbf{N}_i = \mathbf{N}_i(\mathbf{t} + \Delta\mathbf{t}) - \mathbf{N}_i(\mathbf{t}) = \frac{\partial\mathbf{N}_i}{\partial\mathbf{t}}(\mathbf{t} + \Delta\mathbf{t}) \cdot \Delta\mathbf{t} + \sum_j \left(\frac{\partial\mathbf{N}_i}{\partial\mathbf{N}_j} \right) \Delta\mathbf{N}_j$$

- Time integration was carried out until steady state was achieved.

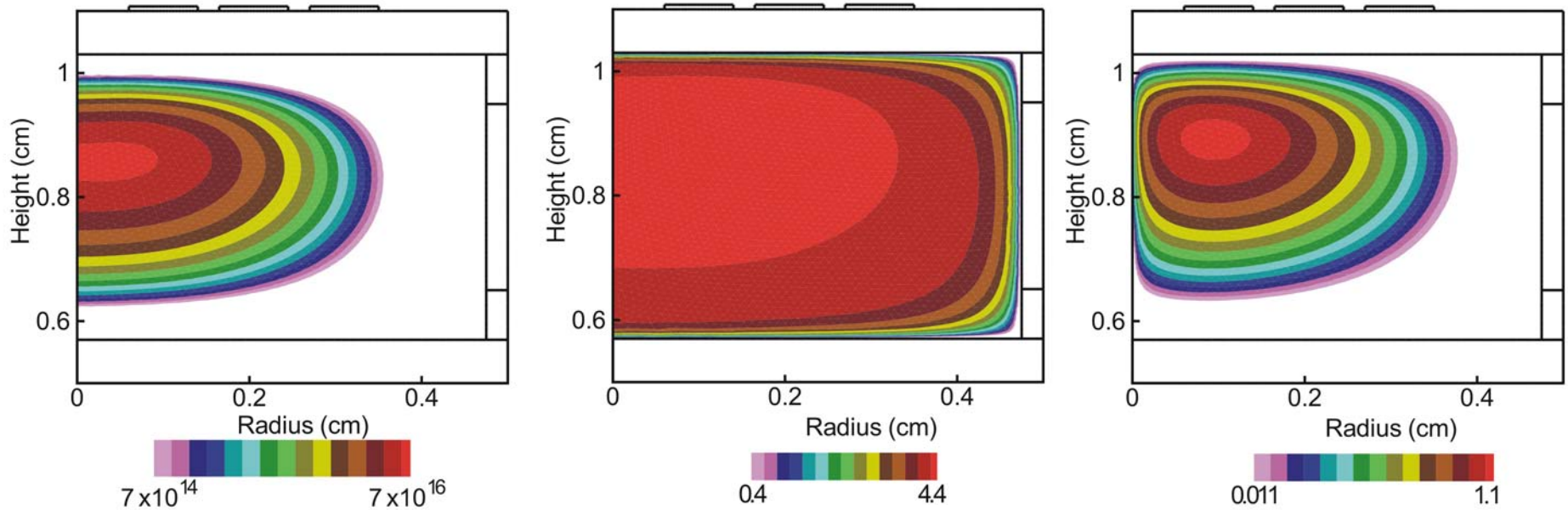
VALIDATION: GEOMETRY AND CONDITIONS

- Investigations of a 2-d cylindrically symmetric micro-ICP reactor were conducted.
- Geometry and conditions were based on Hopwood et. al [1].
 - 500 mTorr, 1 sccm Ar
 - 450 MHz ICP
 - 0.5 – 3.0 Watts(Input)
- Ion densities, and T_e at the center of the reactor (0.0, 0.8 cm) are reported.



[1] J. Hopwood, O.B. Minayeva, Y. Yin, J. Vac. Sci. Tech B, **18**, 2000

VALIDATION: BASE CASE RESULTS

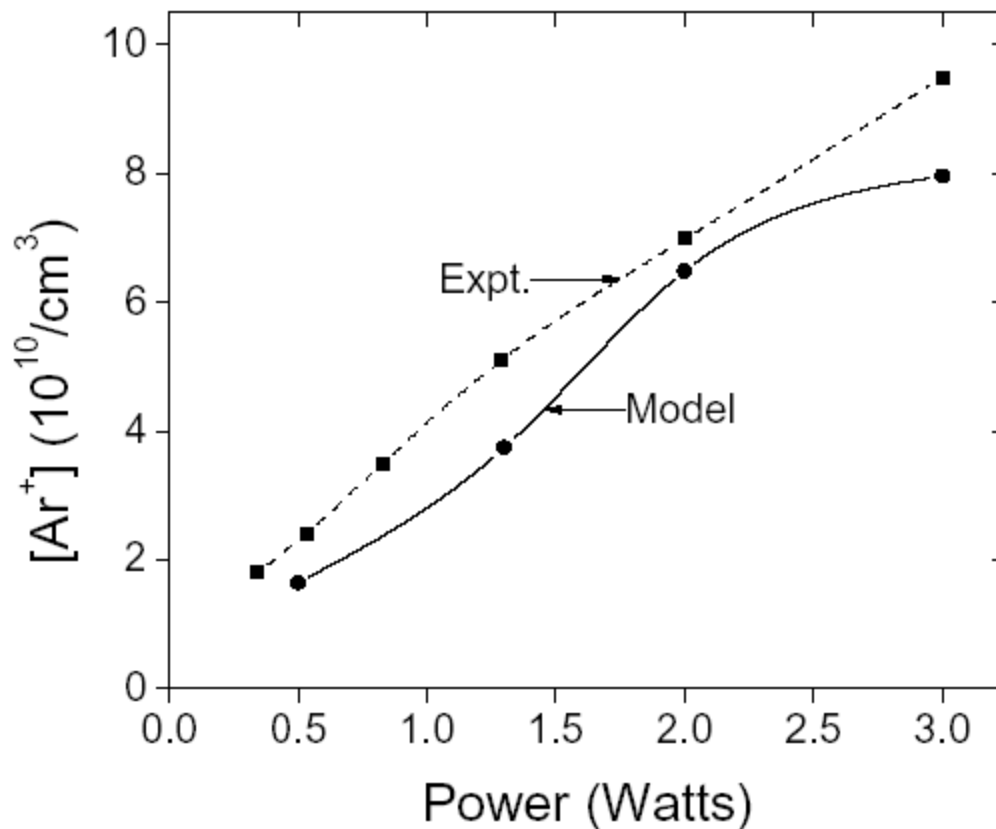


- [e-Source] ($\text{cm}^{-3} \text{s}^{-1}$)
 - T_e (eV)
 - Power (W/cm^3)
- Skin depth of a couple of mm.
 - Debye length of 0.1 mm near the center of the reactor.
 - Operating conditions:
 - 500 mTorr, 1 sccm Ar
 - 1.3 Watts, 450 MHz

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VALIDATION: ION DENSITY

- Ion densities were maximum close to the center of the reactor.
- Power deposited in the plasma was 2.5% of the generator power[2].
- Ion densities of 10^{10} - 10^{11} obtained with power density of $0.1 - 1.0 \text{ W/cm}^3$.
- Lower densities could be attributed to effect of flow.

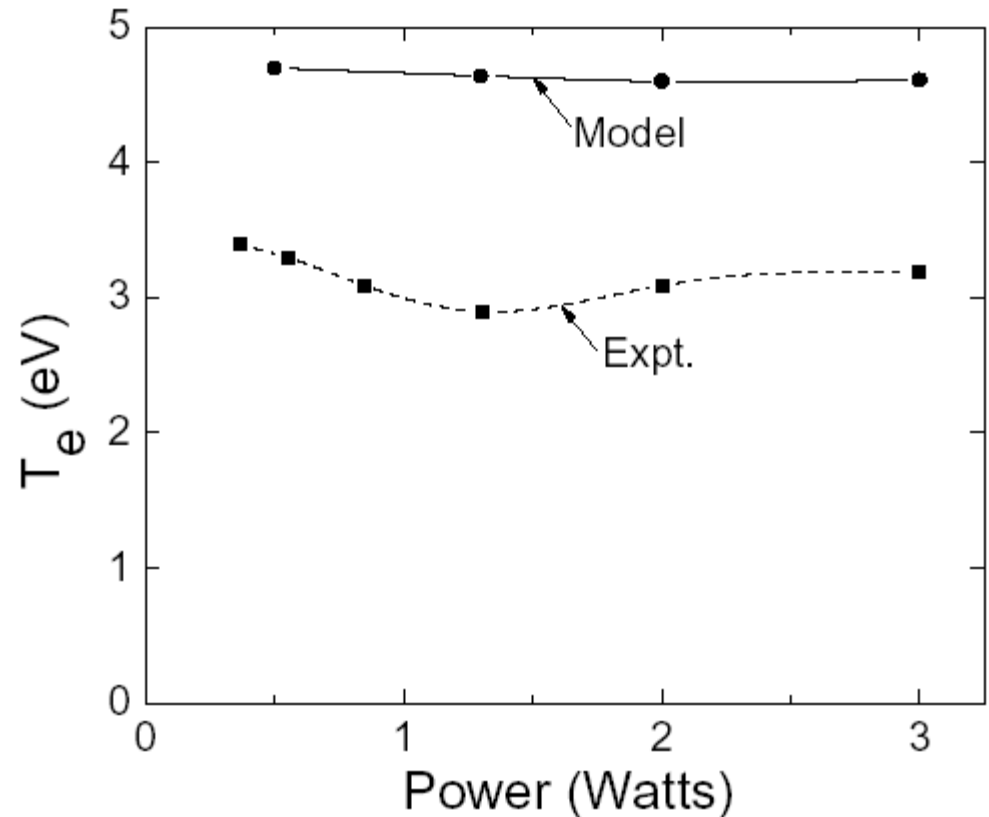


- 500 mTorr, 1 sccm Ar, 450 MHz

[2] O. B. Minayeva and J. Hopwood, J. Appl. Phys. **94**, 2003

VALIDATION: ELECTRON TEMPERATURE

- **Model overpredicts electron temperature.**
- **Model may underpredict multi-step ionization.**

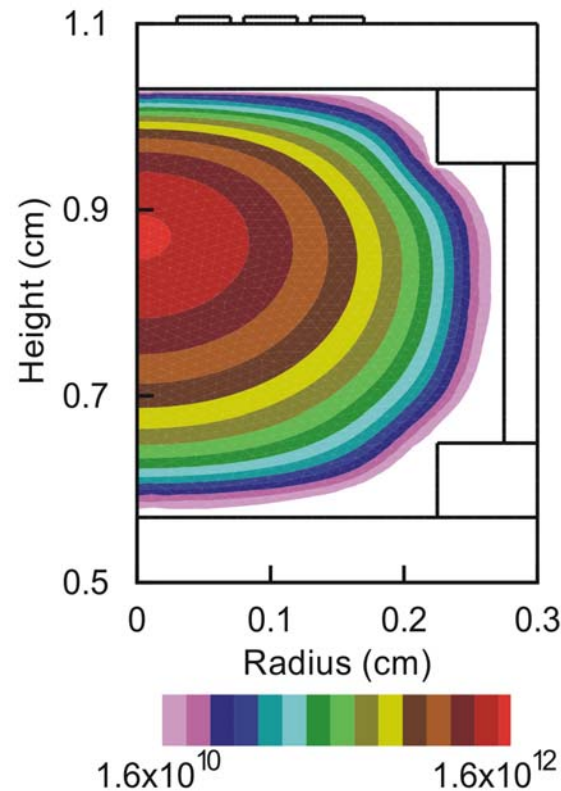


- **500 mTorr, 1 sccm Ar, 450 MHz**
- **Expt: Hopwood, Minayeva, J. Vac. Sci. Tech. B., 18, 2000**

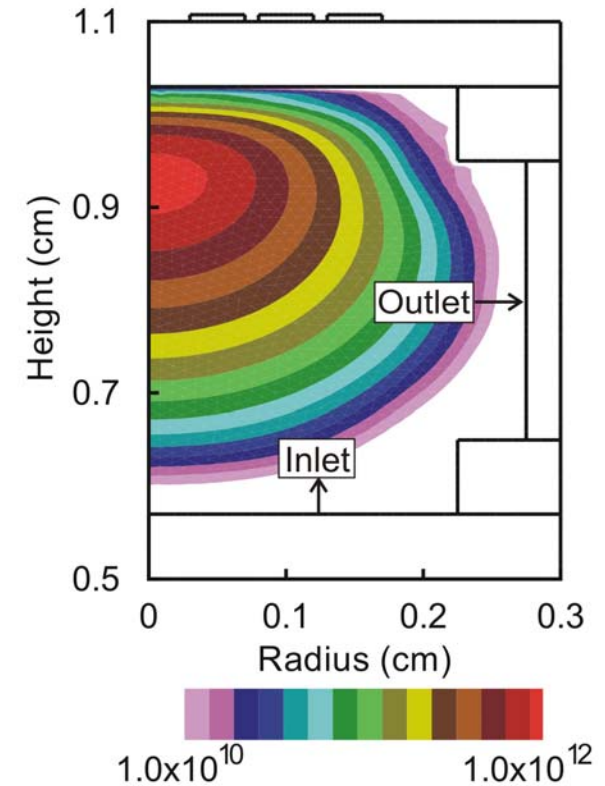
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EFFECT OF FLOW: ION DENSITY

- **Conditions:**
 - 2 Torr, 1.5 Watt
 - 493 MHz ICP
- **Coupling between the ions and the neutrals can affect the ion flux and the flow.**
- **Can be important at higher pressures (>1 Torr) and when there are large gradients in ion densities.**



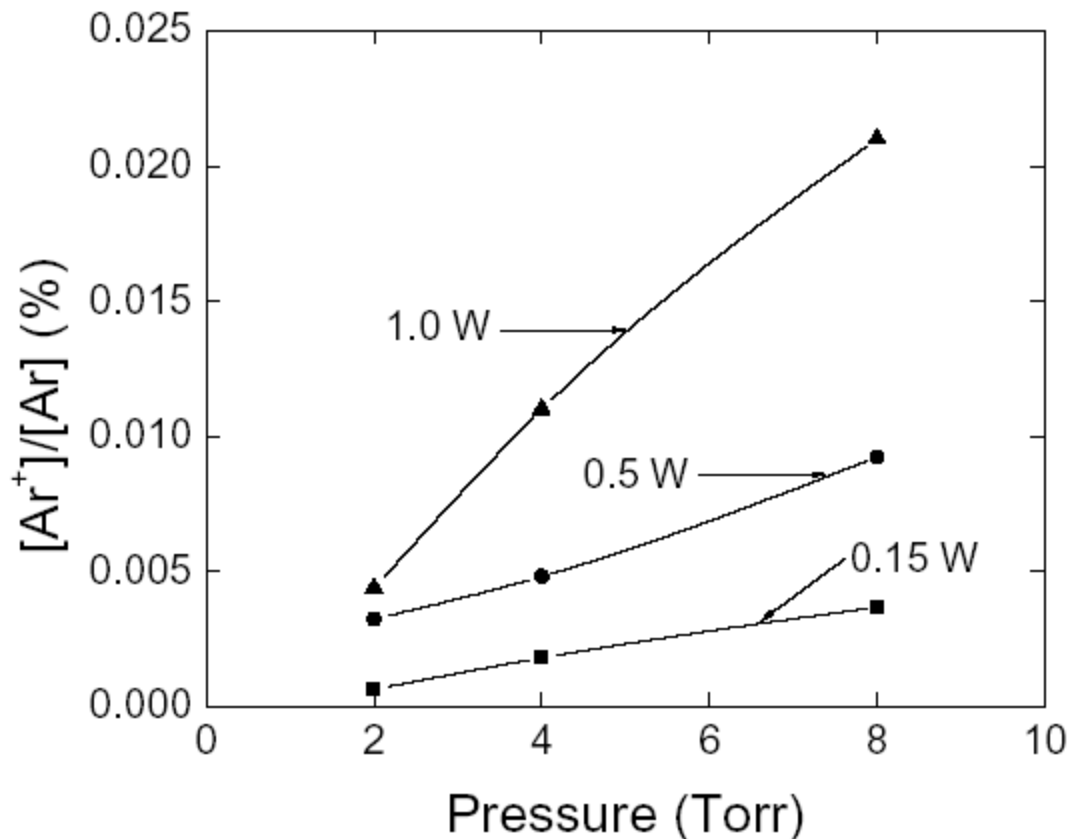
• $[Ar^+]$ without flow



• $[Ar^+]$ with 2 sccm flow

IONIZATION FRACTION

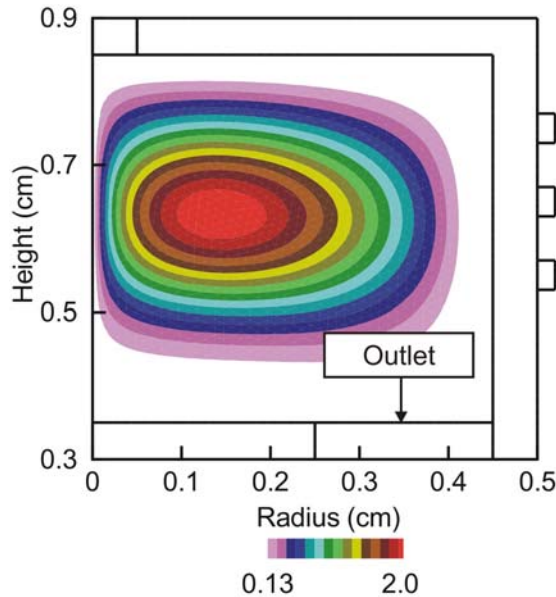
- Ar^+ is the predominant ion as the pressure is too low for Ar_2^+ to efficiently form.
- Ionization fraction increases with pressure.
- Higher ionization than those reported are required for effective use as a thruster.



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EFFECT OF GEOMETRY

Solenoidal

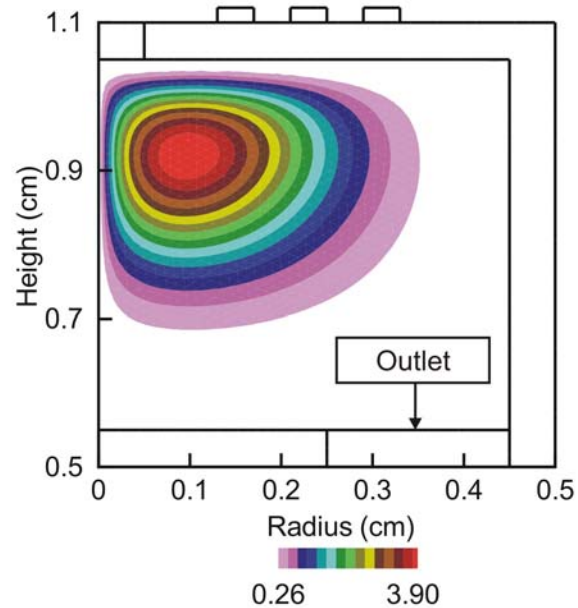


• Power (W/cm^3)

• Conditions:

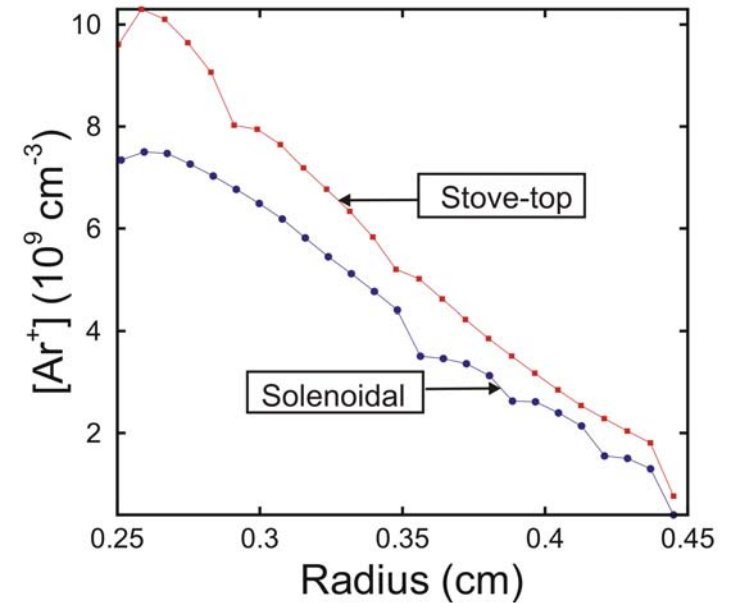
- 2 Torr, 1.5 Watt
- 493 MHz ICP
- 2 sccm Ar

“Stove-top”



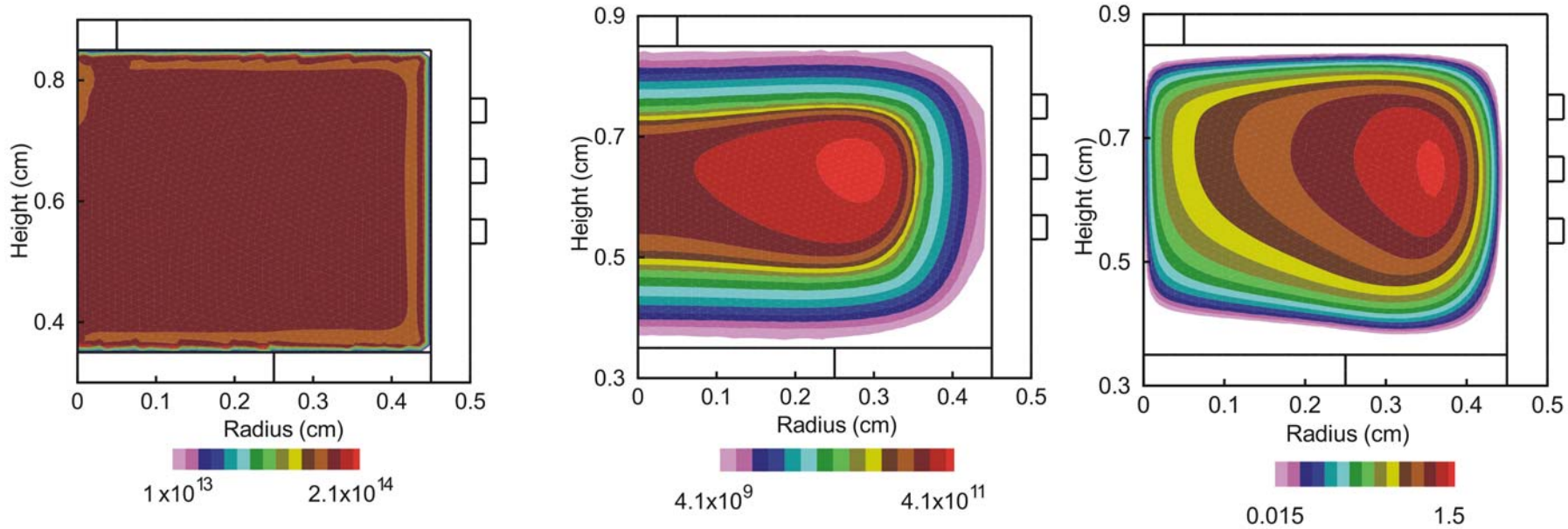
• Power (W/cm^3)

- Power deposition governed by penetration of electric field into the plasma.
- Steeper gradients of species densities caused by nonuniform power deposition affects the flowfield.



• $[\text{Ar}^+]$ at outlet

SOURCES OF ENERGETIC NEUTRALS



- $[O_2(^1\Delta)]$ (cm^{-3})

- $[O_2^+]$ (cm^{-3})

- Power (W/cm^3)

- Conditions:

- 2 Torr, 1.5 Watt
- 493 MHz ICP
- He/O₂ (70:30)
- 10 sccm

- Energetic species such as O₂(¹Δ) can be used in chemical LASERs.
- $[O_2(^1\Delta)] / [O_2] \sim 0.3\%$ is achieved with the current conditions although higher values are required.

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CONCLUSIONS

- Ion densities of 10^{10} - 10^{12} cm^{-3} (ionization fractions of 10^{-5} to 10^{-4}) were generated at modest power levels at pressures ranging from 0.5 - 8 Torr.
- At higher pressures, the momentum transfer between ions and neutrals is important.
- The effect of the geometry of the coils on power deposition and plasma characteristics were studied.
- $[\text{O}_2(^1\Delta)]$ production was simulated using the micro-ICP reactor and $[\text{O}_2(^1\Delta)] / [\text{O}_2] \sim 0.3\%$ was achieved using the base case conditions.