

INVESTIGATION OF AXIALLY FLOWING He/O₂ PLASMAS FOR OXYGEN-IODINE LASERS*

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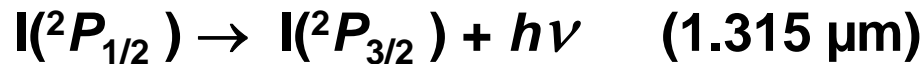
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AGENDA

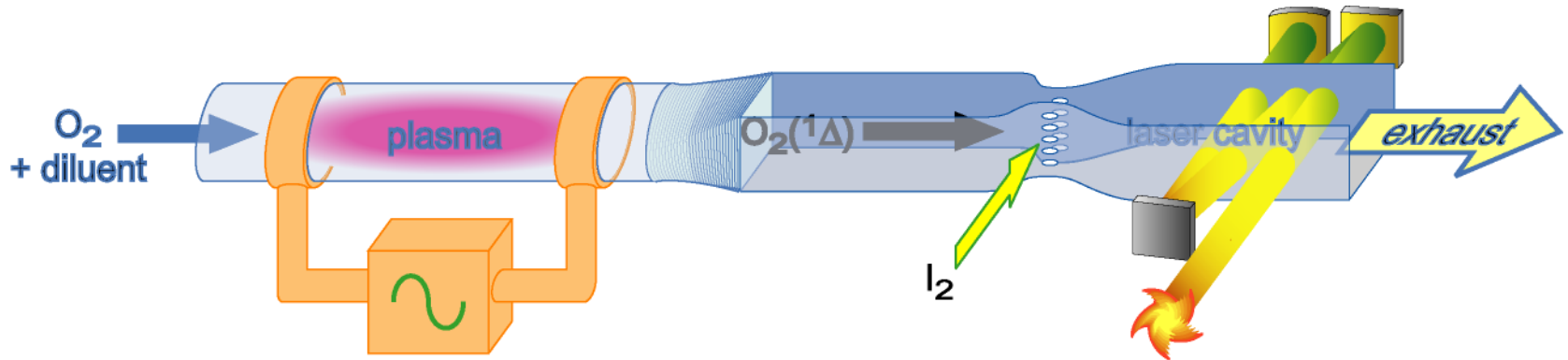
- **Introduction**
 - **Conventional vs. discharge COILs**
 - **Previous modeling**
- **Description of model**
 - **Axial flowing plasma kinetics model**
 - **Reaction mechanism**
- **Results**
 - **Yield scaling with energy deposition**
 - **Axial propagation of plasma zone**
 - **Pulse modulated rf discharges**
- **Conclusion**

OXYGEN-IODINE LASERS

- $O_2(^1\Delta)$ dissociates I_2 and pumps I which lases on the $^2P_{1/2} \rightarrow ^2P_{3/2}$ electronic transition.



- Conventional COILs obtain $O_2(^1\Delta)$ from a liquid phase reaction.
- Electrical COILs obtain $O_2(^1\Delta)$ by exciting O_2 in discharge.



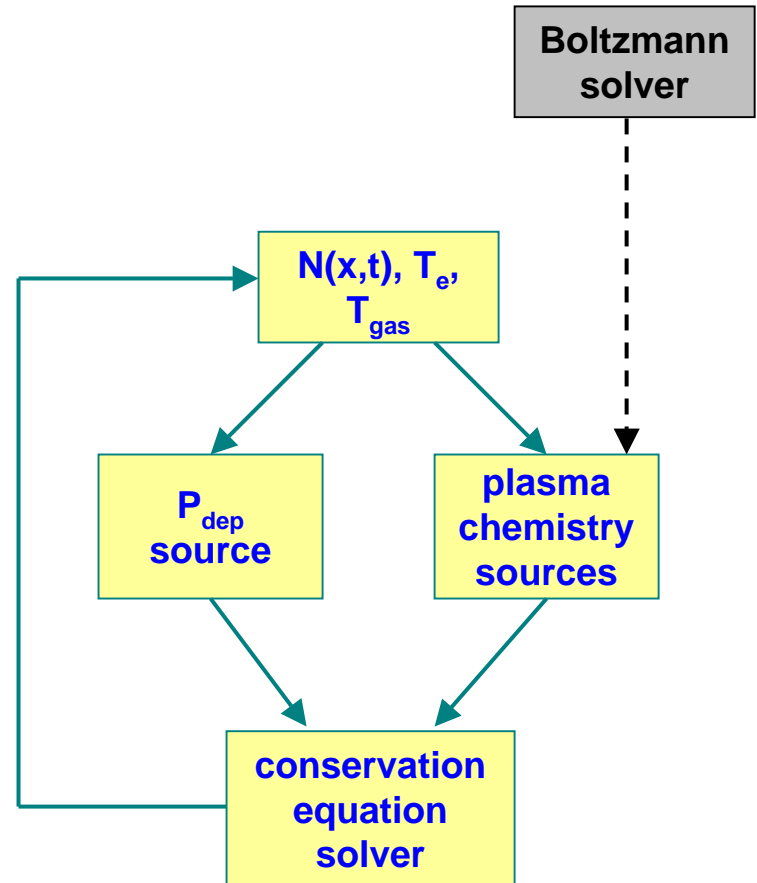
ELECTRIC DISCHARGE COIL MODELING

- **Zero-dimensional plug flow modeling results**
 - **O₂(¹Δ) yield scales with specific energy deposition into O₂ species, peaking near 5–8 eV/molecule.**
 - **Threshold yields of ~15%* have been demonstrated with adequate specific energy deposition.**
- **Further modeling needs**
 - **Axial-transport of species and effect on discharge kinetics.**
 - **Upstream and downstream propagation of the plasma expanding the power deposition zone.**
 - **Differences between CCP and ICP power deposition are difficult to address with 0-D model.**
- **A one-dimensional axial model was developed to address these needs.**

*D. Carroll, *et. al*, Appl. Phys. L. 85(8), 2004.

COMPUTATIONAL SCHEME

- Conservation equations for species densities, gas energy, and electron energy are advanced for 1-D axial flow.
- Source terms are computed by plasma kinetics module.
- Power depositions are computed by CCP and ICP modules.
- Boltzmann solver periodically updates e-impact rate and transport coefficients as a function of position.



AXIAL PLASMA MODEL

- Conservation equations for species densities are solved for a constant mass flux:

$$\rho \vec{v} = \text{const.} \quad \frac{\partial N_i}{\partial t} = -\nabla \cdot \left[N_i \left(\vec{v} + \vec{v}_{diff,i} + \vec{v}_{drift,i} \right) \right] + S_i + W_i$$

- Drift velocities are obtained by calculating the axial ambipolar electric field:

$$\vec{E}_a = -\frac{\sum_i q_i N_i \vec{v}_{diff,i}}{\sum_i q_i^2 \mu_i N_i}$$

- Gas and electron energy equations are integrated:

$$\rho c_p \frac{\partial T}{\partial t} = -\rho \vec{v} c_p \cdot \nabla T - \nabla \cdot \vec{q} - \tau_{zz} \nabla \cdot \vec{v} + \frac{Dp}{Dt} + \frac{\kappa}{\Lambda^2} (T_{wall} - T_{gas}) + \Delta h_{rxn} + h_e$$

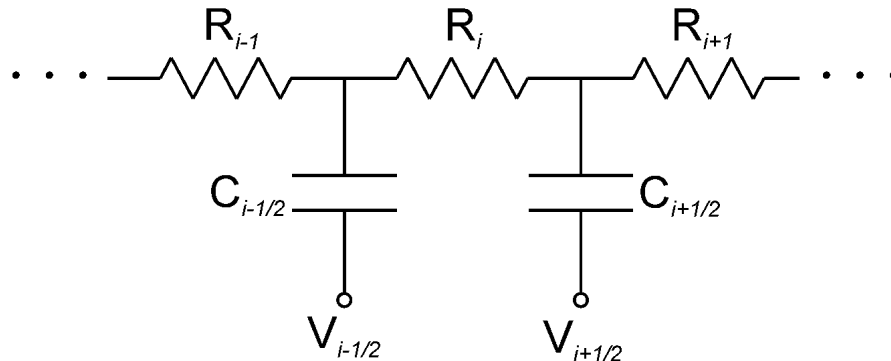
$$\frac{\partial \left(\frac{3}{2} n_e k_B T_e \right)}{\partial t} = -\nabla \cdot \vec{q}_e + P_d - h_e + \sum_l n_e k_l N_l \Delta \varepsilon_l$$

POWER DEPOSITION MODELS

- ICP module estimates axial magnetic field from coils wound on discharge tube and includes skin depth effect:

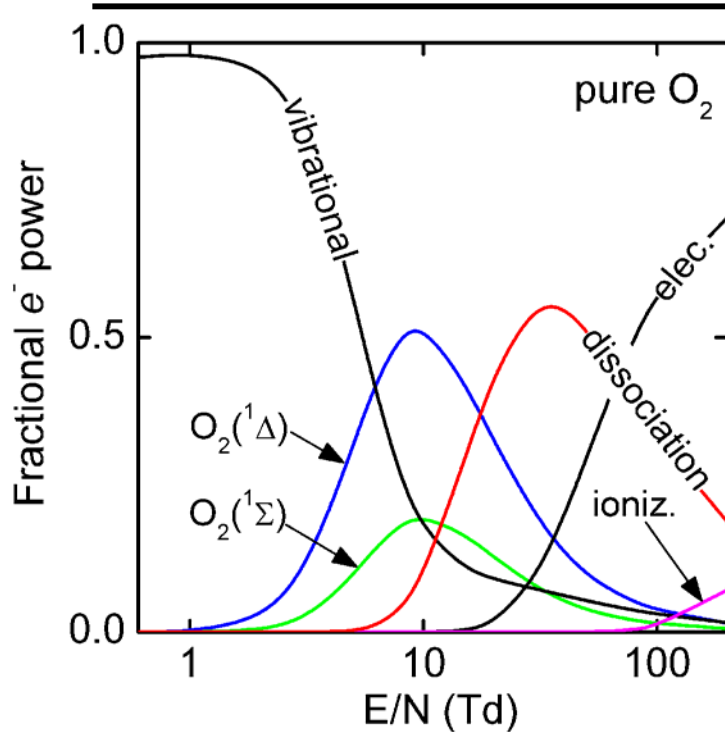
$$B_i = \sum_j^N \frac{2\mu_0 R^2 I}{4r_{ij}^3} \exp\left(\frac{-r_{ij}}{\delta_{ij}}\right)$$

- CCP module models the discharge as a transmission line, where each grid point represents a node:



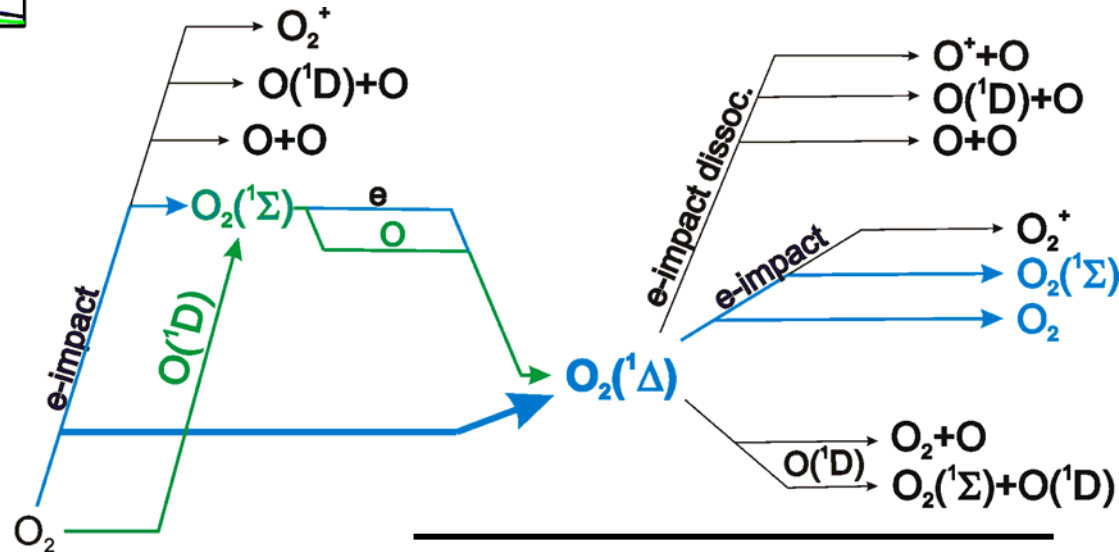
$$P_{d,i} = \Re\left(\frac{V_{R,i} V_{R,i}^*}{R_i}\right)$$

REACTION MECHANISM



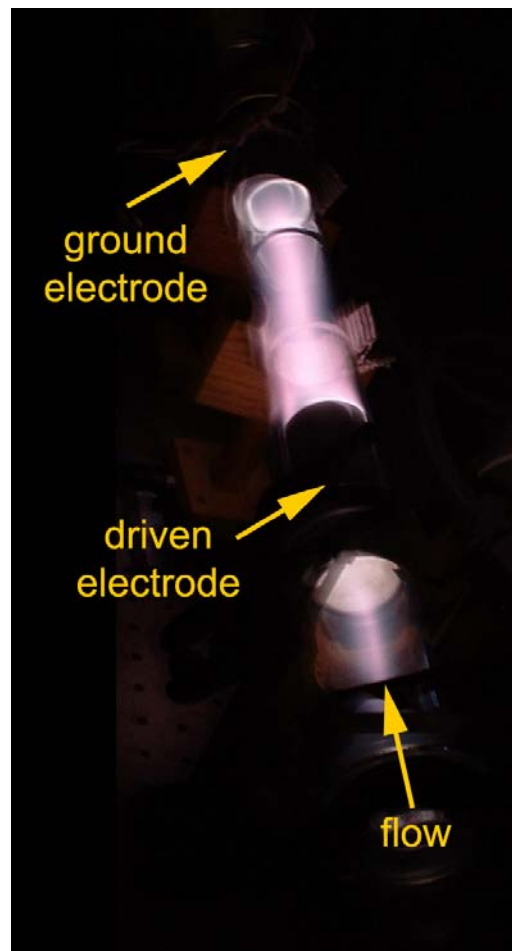
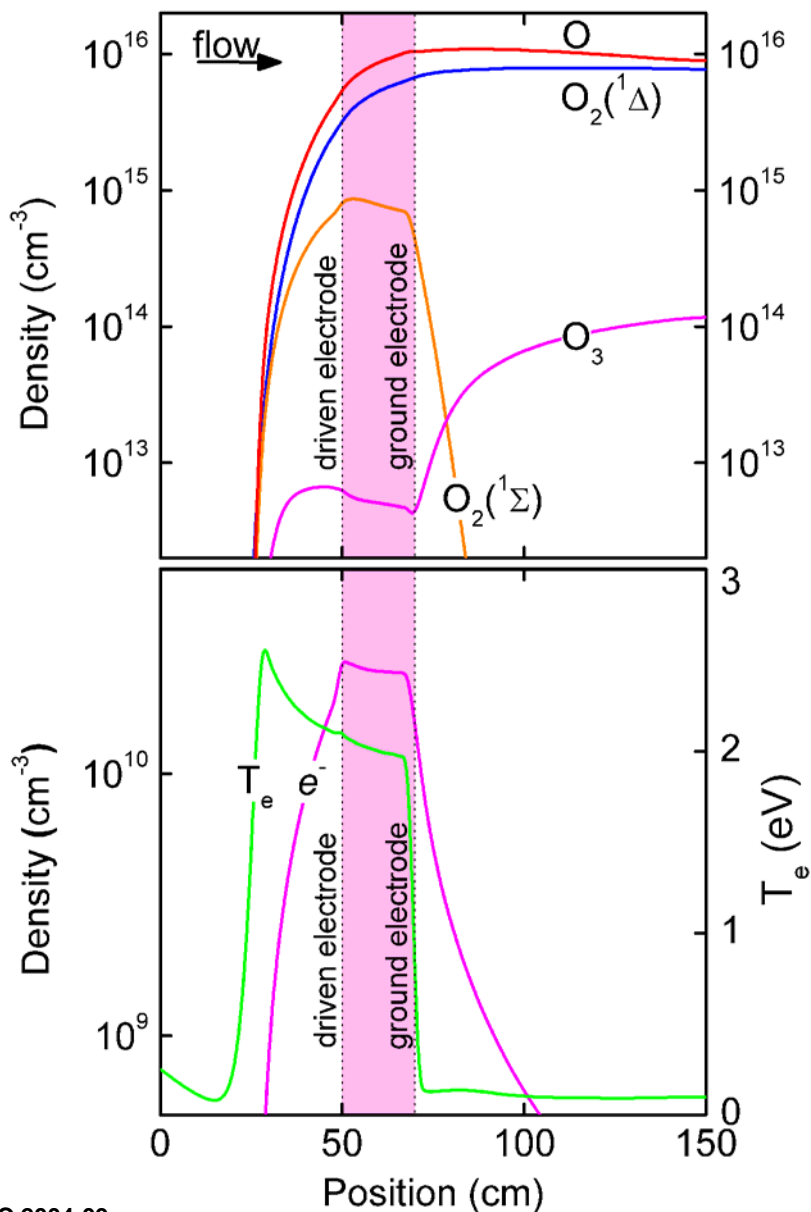
- Discharge kinetics are dominated by e-impact excitation of $O_2(^3\Sigma)$ to $O_2(^1\Delta)$, and by excitation and dissociation of $O_2(^1\Delta)$.

- Recent efforts have focused on reducing the operating E/N to improve efficiency of $O_2(^1\Delta)$ production.



BASE CASE: ElectriCOIL EXPERIMENT

20 mmol/s of He/O₂=8/2 at 10.6 Torr.
Power = 340 W CCP at 13.56 MHz.

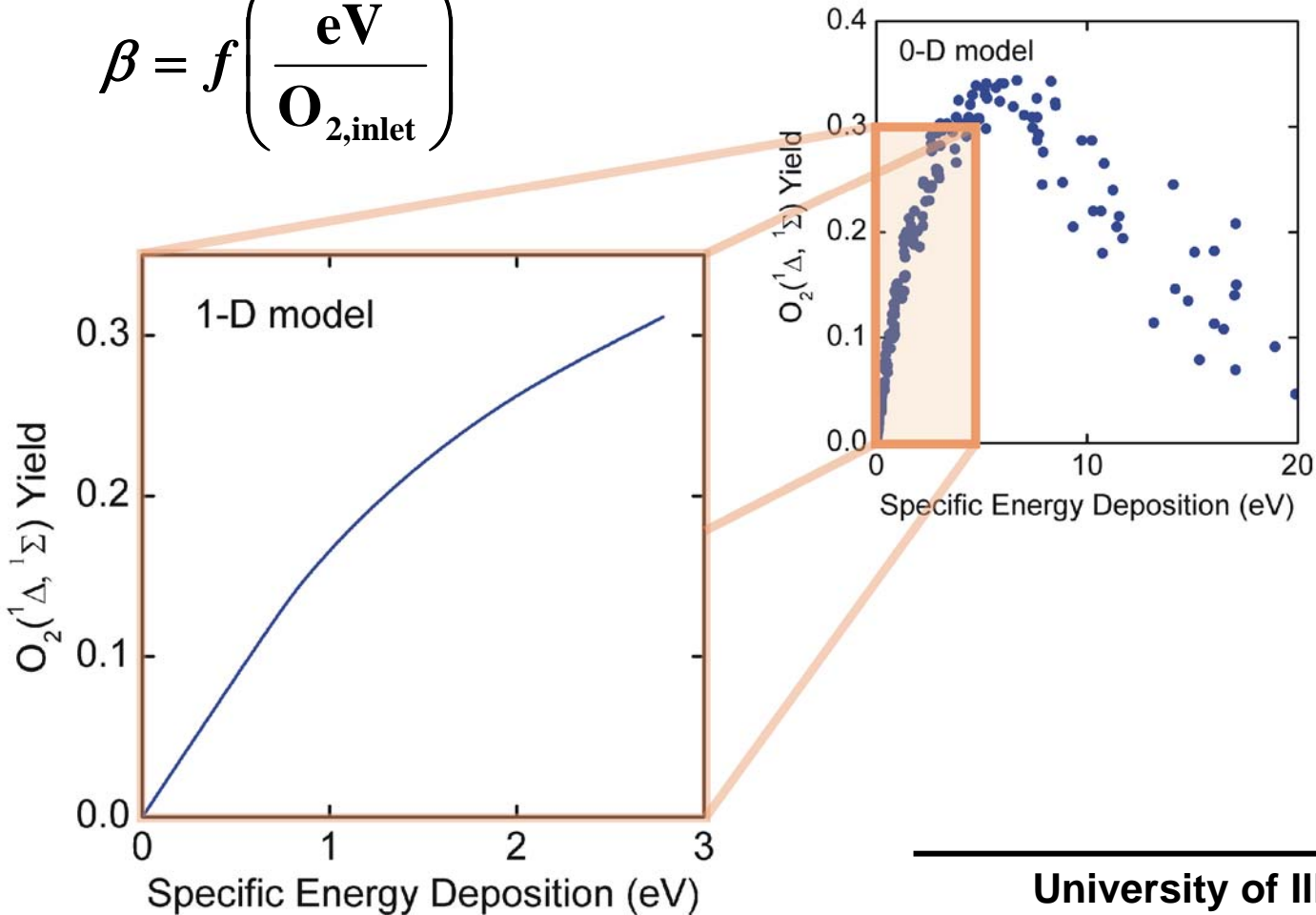


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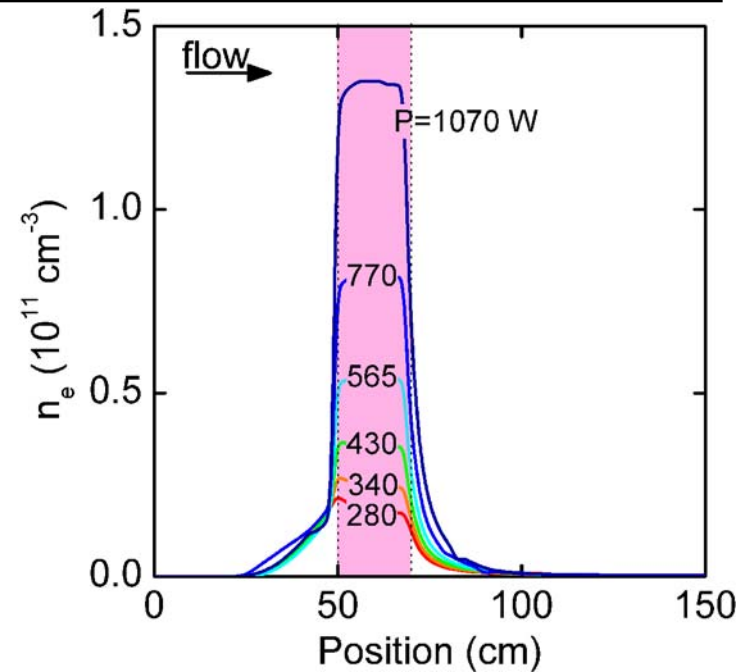
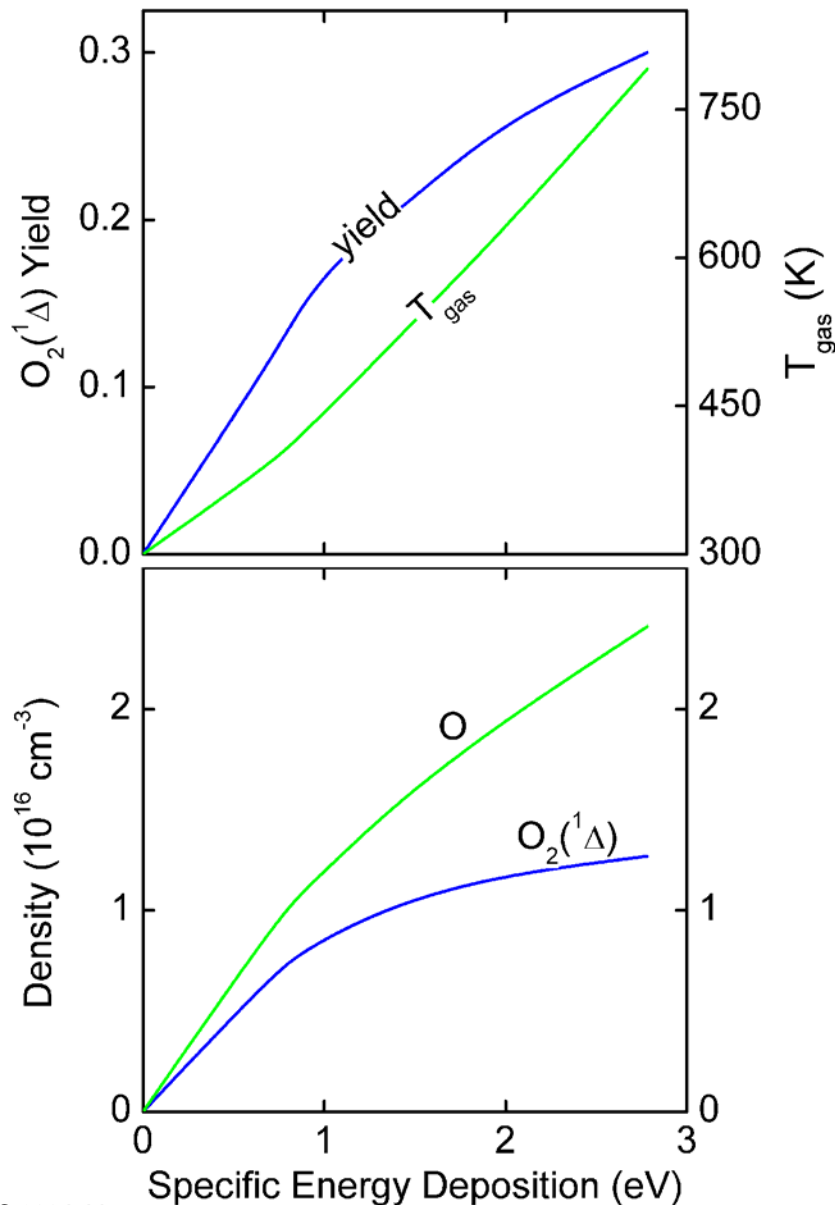
SPECIFIC ENERGY DEPOSITION SCALING

- $O_2(^1\Delta)$ yield scales with specific energy input to O_2 species as predicted by 0-D model.

$$\beta = f\left(\frac{eV}{O_{2,inlet}}\right)$$

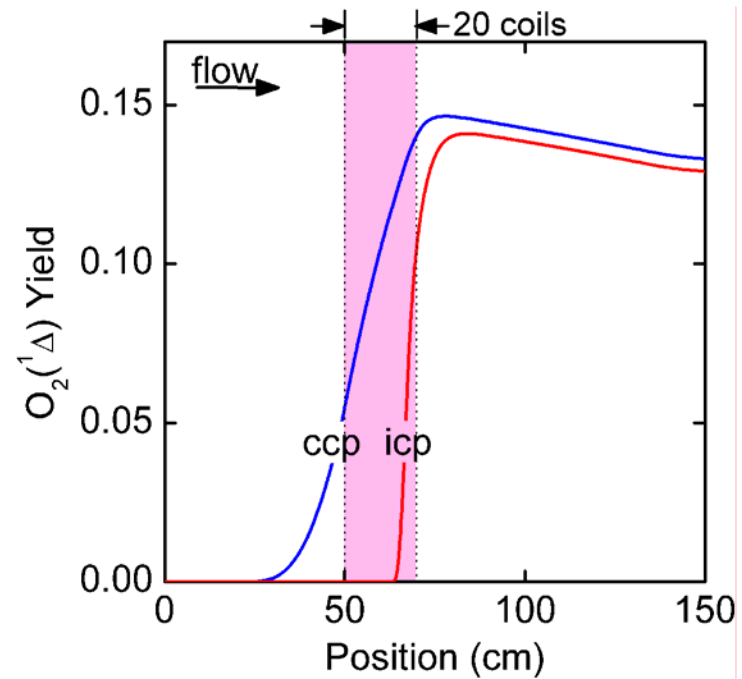
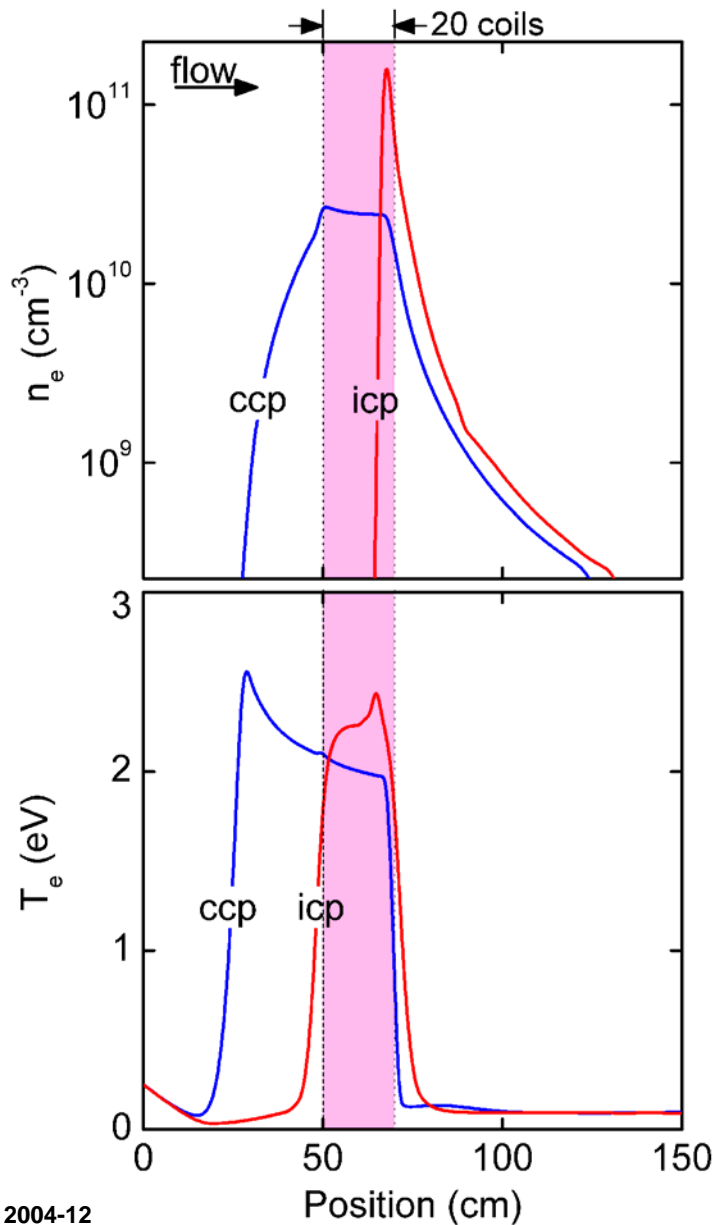


EFFECT OF CCP POWER



- Dissociation increases at large specific energy, reducing the efficiency of $O_2(^1\Delta)$ production.
- Increased conductivity causes plasma zone to spread at higher powers.

ICP vs CCP



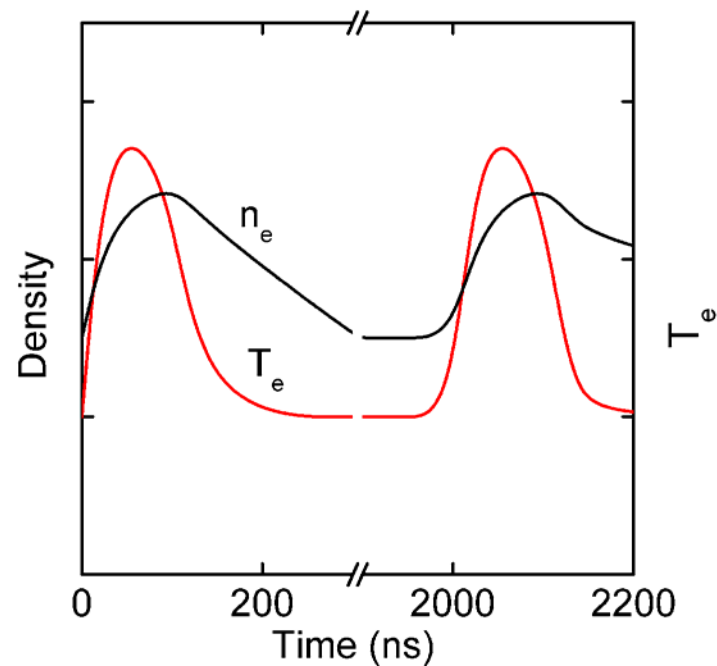
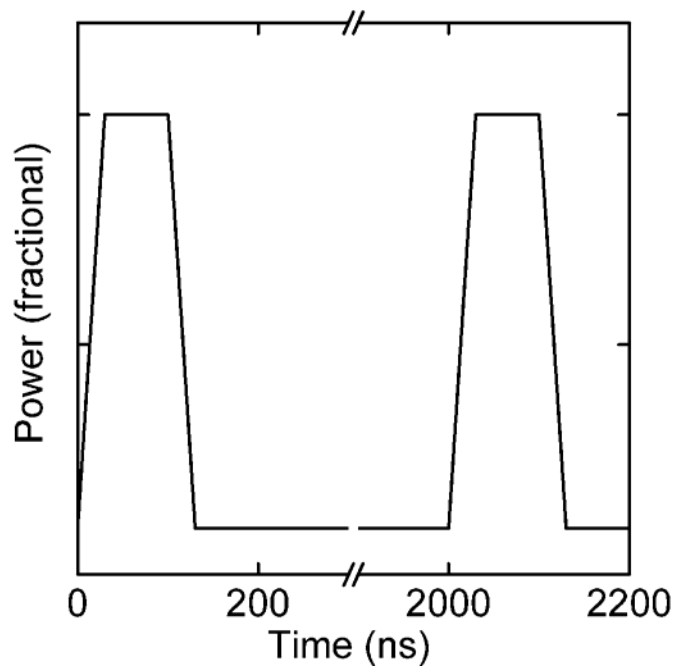
- **CCP T_e , n_e maximize production rate of $O_2(^1\Delta)$ relative to ICP:**

$$\text{rate} \propto \int_{\text{distance}} n_e(x) k_{\text{rate}}(T_e(x)) dx$$

**20 mmol/s, He/O₂=8/2 at 10.6 Torr.
Power = 340 W (0.88 eV/molecule).**

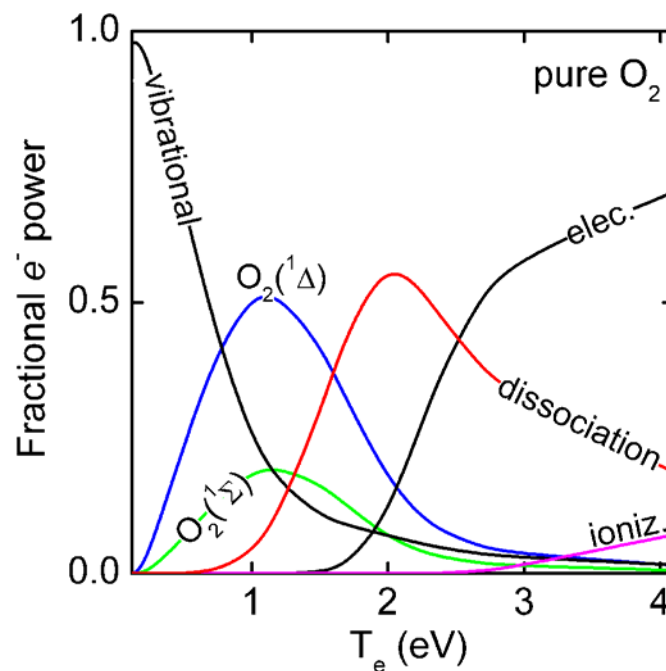
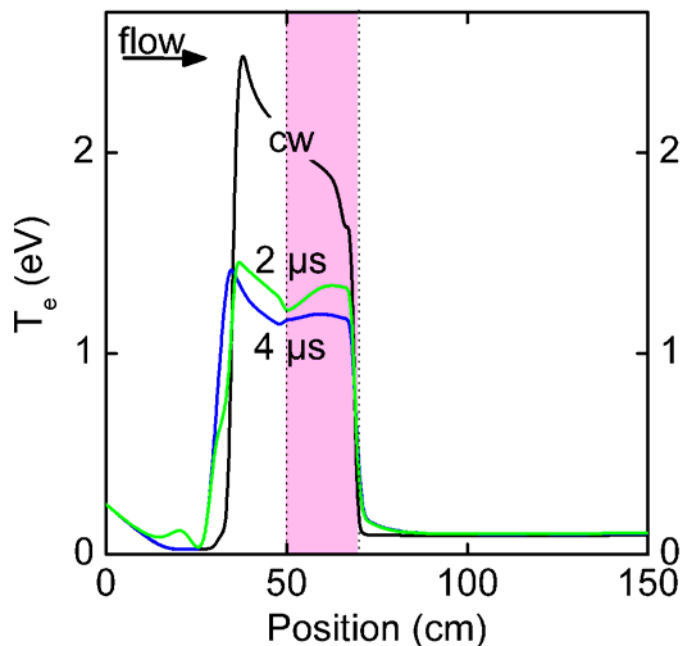
PULSED CCP

- Pre-ionizing the plasma with a high power pulse allows discharge to operate below the self-sustained E/N, nearer to the optimal E/N for $O_2(^1\Delta)$ production.
- Overall efficiency of pre-ionization depends on the extent of pre-ionization and the delay between pulses.



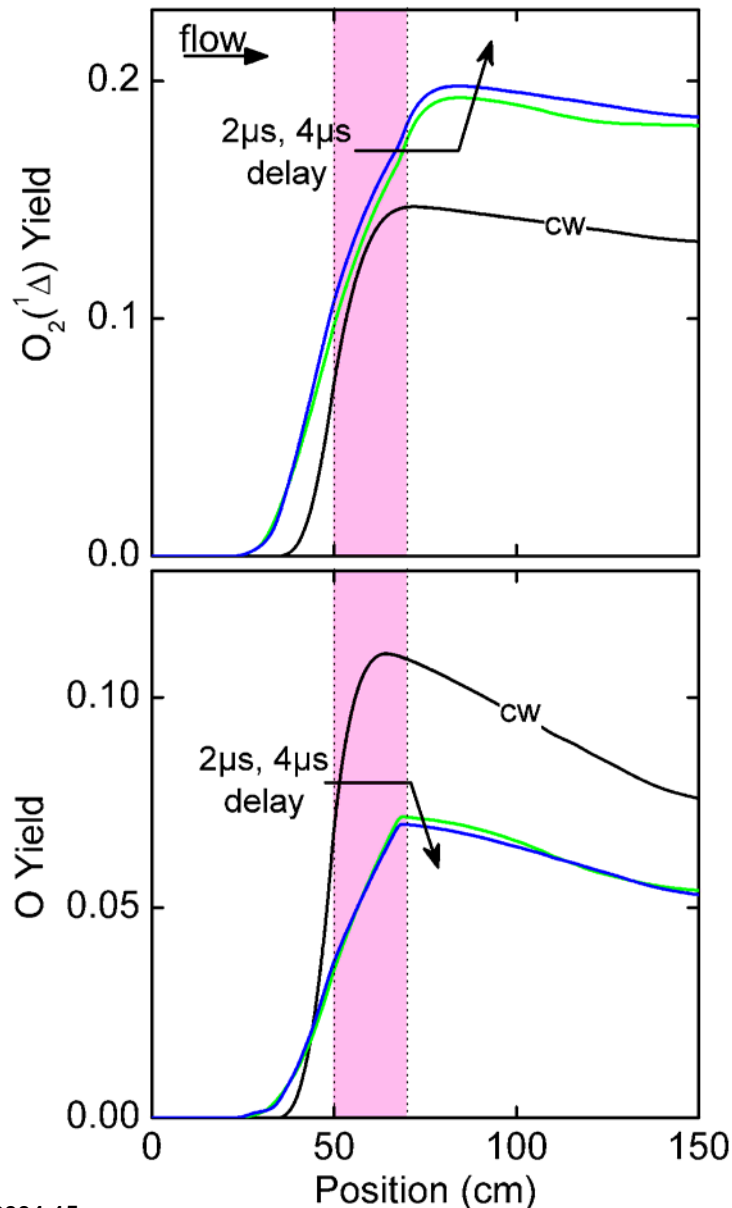
PULSED CCP: PULSE DELAY & AMPLITUDE

- Average T_e of pulsed discharge is reduced ≈ 1 eV relative to cw discharge.
- In cw discharge T_e is optimal for dissociation, but in pulsed discharge T_e is optimal for $O_2(^1\Delta)$ production.



20 mmol/s, He/ O_2 =8/2 at 10.6 Torr.
Peak 2.5 kW, avg. 340 W CCP at 100 MHz.

PULSED CCP vs. CW



- Modest pulsing schemes significantly outperform cw discharges at these conditions.

- Pulsing reduces the average T_e (and E/N), increasing $O_2(^1\Delta)$ production and reducing dissociation to O atoms.

20 mmol/s, He/ O_2 =8/2 at 10.6 Torr.
Peak 2.5 kW, avg. 340 W CCP at 100 MHz.

CONCLUSIONS

- A 1-D axially flowing discharge model was developed to investigate the effects of axial transport on $O_2(^1\Delta)$ yields.
- Conservation equations for species densities, gas energy, and electron energy were solved.
- $O_2(^1\Delta)$ yield in rf ICP and CCP discharges was found to scale with specific energy deposition into O_2 species.
- CCP discharges produced somewhat higher $O_2(^1\Delta)$ yields than ICP discharges due to their broader power deposition zone.
- Pulsed discharges using a high power pre-ionizing pulse produced the highest yields, $\approx 50\%$ higher than CCP, by reducing the T_e below the self-sustaining value.

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